

PATENT SPECIFICATION

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(54) WEAR-RESISTANT CAST-IRON ALLOY

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 SCHAFT, a Body Corporate organised and
 existing under the laws of the Federal Re-
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 many, do hereby declare the invention, for
 which we pray that a patent may be granted
 to us, and the method by which it is to be
 performed, to be particularly described in
 and by the following statement:—

The present invention relates to a wear-
 resistant cast iron alloy suitable for the con-
 struction of machine parts subject to high
 frictional stresses.

Machine elements subjected to friction are
 strongly stressed both with regard to wear
 and thermally, so that particularly high
 demands have to be made on their materials.
 Certain machine elements, such as the piston
 rings of internal combustion engines and the
 sealing strips of rotary piston engines, are
 furthermore subjected to particularly heavy
 stresses. Experience has shown that only very
 expensive materials of complicated manufac-
 ture withstand such high stresses. Usually,
 these materials are sintered metal carbides,
 to which very specific alloying elements have
 been added.

The sorts of cast iron so far tested, how-
 ever, cannot be used for these highly stressed
 machine parts. It is known that the wear

resistance of cast iron can be increased by
 the addition of alloying elements. On solidifi-
 cation of the cast iron, however, these ele-
 ments form relatively coarse grains and very
 hard carbides, which then cause damage,
 accompanied by scoring, to the contacting
 surfaces. At the same time, carbide formation
 uses up the greater part of the carbon, so that
 these alloys do not contain in their structure
 the necessary graphite for emergency run-
 ning of machine elements. Furthermore, these
 materials are so brittle that they are unable
 to withstand mechanical stresses and there-
 fore break.

In accordance with the present invention
 there is provided a wear-resistant cast iron
 alloy, suitable for the construction of machine
 parts subject to high frictional stresses, the
 alloy containing

1.5 to 4.0% by weight of carbon
 1.5 to 6.0% by weight of silicon
 less than 0.2% by weight of sulphur
 less than 2.5% by weight of phosphorus
 1.0 to 7.0% by weight of copper
 0.4 to 3.2% by weight of nickel and/or
 cobalt
 0.1 to 1.8% by weight of tin and/or anti-
 mony
 0.1 to 4.0% by weight of molybdenum
 0.1 to 4.0% by weight of tungsten
 0.05 to 2.5% by weight of manganese

	0.3 to 2.5% by weight of chromium	0.9% by weight manganese	
	0.3 to 4.0% by weight of vanadium	0.4% by weight chromium	65
	0 to 2.0% by weight of titanium	1.5% by weight vanadium	
5	0.1 to 4.0% by weight of niobium and/or tantalum	0.2% by weight titanium	
	0.1 to 2.0% by weight of aluminium	0.7% by weight niobium	
		0.01% by weight boron	70
		0.22% by weight aluminium	
	and the rest iron except for atmospheric nitrogen combined with the metals as a result of melting and heat treatment.	and the rest iron.	
10	The cast iron alloys in accordance with the invention display uncombined carbon as lamellar and primarily nodular precipitates. There are also present however a large number of carbides in a very fine crystalline precipitated form.	After inoculation with one of the usual inoculants, sealing strips for rotary piston engines were cast from the melt using the sand mould casting process, the dimensions of the strips being 61.03×8.3×4.95 mm. They were then annealed for one hour at 850°C, quenched in an oil bath at room temperature and tempered for one hour at 350°C.	75
15	The sum of the elements carbon and silicon in the alloys in accordance with the invention is equal to or greater than 3% by weight and the ratio of silicon to carbon is preferably equal to or greater than one. The sum of the elements molybdenum, tungsten and manganese should preferably be between 0.2 and 10% while the sum of the elements chromium, vanadium, tantalum and niobium should preferably be between 1 and 10%.	The sealing strips thus made had an HV 5 hardness of 644 to 713 kg/mm ² . In test runs, the sealing strips showed very good wear resistance, while the trochoidal running surfaces were only slightly affected.	80
20	In addition, it has been found that for refining the form of the individual structural constituents, more particularly that of the graphite, and the nitrides (when present), the elements boron, bismuth, zirconium, magnesium and/or the rare-earth metals may be added. Their total concentration should not, however, exceed the value of 0.5 percent by weight.	Figures 1 to 4 show photomicrographs of the cast-iron alloy of the example.	85
25	By heat treatment above 700°C, followed by quenching for example in air or a salt bath to a temperature of below 500°C, and subsequent tempering up to a temperature of 700°C, wear resistance and compatibility with the counter-material are greatly increased.	Figure 1 is the unetched specimen at a magnification of ×100, showing the graphite in lamellar to nodular form.	
30	The alloys according to the invention have a bainitic to martensitic basic structure. The graphite precipitates are lamellar to nodular, the carbide precipitates are punctiform to spherical. The hardness of this material at HV 5 lies at 550 to 920 kg/mm ² . The material is not brittle and cast sealing strips for rotary piston engines are wear resistance and in test runs exhibit very good wear resistance with the trochoidal surface of the rotary piston engine.	Figure 2 is the unetched specimen at a magnification of ×500, showing in addition to the dark graphite precipitates, the finely crystalline carbide constituents as light areas with a dark edge.	90
35	The embodiment example describes one of the cast-iron alloys according to the invention. The cast-iron melt comprises the elements	Figure 3 shows a specimen etched with HNO ₃ at a magnification of ×500 which shows, in addition to the graphite precipitates and the crystalline carbide constituents, the bainitic to martensitic structure.	95
40		Figure 4 shows the phosphide eutectic, deeply etched, at a magnification of ×20.	100
45		WHAT WE CLAIM IS:—	
50		1. A wear resistant cast iron alloy, suitable for the construction of machine parts subject to high frictional stresses, the alloy containing	105
55	2.2% by weight carbon	1.5 to 4.0% by weight of carbon	
	3.9% by weight silicon	1.5 to 6.0% by weight of silicon	
	0.9% by weight phosphorus	less than 0.2% by weight of sulphur	
	0.08% by weight sulphur	less than 2.5% by weight of phosphorus	110
	1.4% by weight copper	1.0 to 7.0% by weight of copper	
60	0.6% by weight nickel	0.4 to 3.2% by weight of nickel and/or cobalt	
	0.2% by weight tin	0.1 to 1.8% by weight of tin and/or antimony	115
	1.5% by weight molybdenum	0.1 to 4.0% by weight of molybdenum	
	3.4% by weight tungsten	0.1 to 4.0% by weight of tungsten	
		0.05 to 2.5% by weight of manganese	
		0.3 to 2.5% by weight of chromium	120
		0.3 to 4.0% by weight of vanadium	
		0 to 2.0% by weight of titanium	
		0.1 to 4.0% by weight of niobium and/or tantalum	
		0.1 to 2.0% by weight of aluminium	

and the rest iron except for atmospheric nitrogen combined with the metals as a result of melting and heat treatment.

- 5 2. An alloy as claimed in Claim 1 modified by the addition of up to 0.5% by weight in total of one or more of the elements boron, bismuth, magnesium, zirconium and rare earth metals.

3. An alloy as claimed in Claim 1 or 2

which has been subjected to heat treatment by annealing above 700°C, quenching to below 500°C and then tempering up to a temperature of 700°C. 10

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1482724 COMPLETE SPECIFICATION

1 SHEET This drawing is a reproduction of
the Original on a reduced scale

FIG. 1

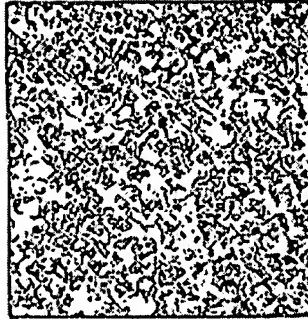


FIG. 2



FIG. 3

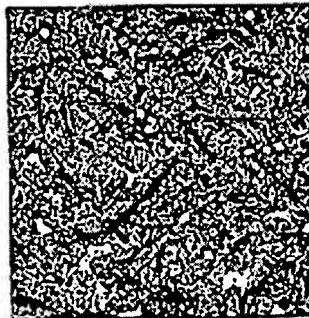


FIG. 4

